

### F&J SPECIALTY PRODUCTS, INC.

PO Box 2888 Ocala, Florida 34478-2888 **Tel:** (352) 680-1177 • (352) 680-1178

**Fax:** (352) 680-1454

The Nucleus of Quality Air Monitoring Programs

### RADIOIODINE COLLECTION FILTER EFFICIENCY TESTING PROGRAM

at

F&J SPECIALTY PRODUCTS, INC.

by

FRANK M. GAVILA

12<sup>th</sup> Annual RETS/REMP Workshop

Atlantic City, New Jersey 24-26 June 2002

Rev: 30 May 2002

### **Table of Contents**

			Page
I.	Radioiod Program	line Collection Cartridge Efficiency Testing	1 - 2
	O	pical Geometries	
		pical Adsorbents utilized in Cartridges	
	• •	oduct Specifications	
II.	Standard	dized Testing	3-5
		TM D 3803, 1989	
		npling Scenarios	
		alysis of Test Data	
III.	Factors A	Affecting Efficiencies of Radioiodine Collection ges	6
IV.	F&J Qua	ality Assurance and Quality Control Program	7
Apper		, D: . D:	
		ter Dimension Diagrams	
		rticle Size Selector Chart	
		pical Product Specifications	
		pical Equations for Efficiency vs. Flow Rate	
	• •	pical Pressure vs. Flow Rate Data	
	• •	pical Quality Control Data Collected Regularly ring Production	
		pical Defect Analysis Data Collection Sheet	
		1-1 and A-2	
	-	-1 and B-1	
	Graph C		

#### I. Radioiodine Collection Cartridges Efficiency Testing Program

The key elements of the F&J quality assurance program for the manufacture of TEDA impregnated charcoal and silver zeolite cartridges utilized in the collection of airborne radioactive iodine species in power plant atmospheres include the following:

- 1. Testing is performed on every batch of adsorbent material
- 2. Testing is performed at different flow rates in order to have representative data across the flow range utilized by power plant personnel.
- 3. Integration of new batch data from individual batches into data of all previous batches.
- 4. Development of data for different sampling scenarios
- 5. Determination of "Pressure Drop" data vs. flowrate for each type of adsorbent material.
- 6. Creation of graphical representation of the collection efficiency vs. flow data and determination of mathematical equations that represent the efficiency vs. flow relationship.

Eighty percent (80%) of testing is performed on the filter geometries that represent 80% of the production quantity.

Radioiodine Collection Cartridges are available in various geometries, contain various adsorbents, and the specific adsorbents are available in various mesh sizes. Typical cartridge geometries available from F&J are listed in Table I below:

TABLE I
RADIOIODINE COLLECTION FILTER GEOMETRIES

<b>Nominal Dimensions</b>	<u>Material</u>	F&J Geometry
2 1/4"D ×1" H	Plastic Cased	C, CS and CSM Series
2 1/4"D ×1" H	Plastic Cased	B Series
2 1/4"D ×1" H	Metal Cased	M Series
2 1/4"D ×1" H	Metal Cased	M.5 Series (WGRM Monitor)
$3.43"D \times 1.23"H$	Plastic Cased	3X1 Series
3.2"D × $2.2$ "H	Plastic Cased	3X2 Series
$1.63"D \times 0.76"H$	Plastic Cased	Lapel Filter Series
1.24"D × $1.11$ "H	Plastic Cased	744/844 Series (Victoreen Monitor)

Refer to the filter dimension diagrams in Appendix A.

Typical adsorbents that may be utilized in the various geometries listed in Table I above are listed in Table II below:

TABLE II
TYPICAL ADSORBENTS AND MESH SIZES AVAILABLE

TEDA Impregnated Carbon (5% by Wt. TEDA)		Silver Zeolite (37% by Wt. AG.)	Silver Impregnated Silica Gel (12% by Wt. AG.)				
	U.S. Sieve	U.S. Sieve	U.S. Sieve				
TEDA-1	8×16	16×40	10×16				
TEDA-2	30×50	30×50					
TEDA-3	20×40	50×80					
TEDA-4	12×20						

Refer to Appendix B for a graphical representation of particle sizes.

### **Product Specifications**

Each Radioiodine Collection Cartridge manufactured by F&J has detailed specifications indicating physical and performance specifications for the product. A typical set of specifications for a TEDA impregnated charcoal cartridge and a silver zeolite cartridge is presented in Appendix C.

#### II. Standardized Testing

Utilization of these filters (or any other filters) requires determination of an efficiency value for the physical conditions typically experienced during field sampling operations. Physical parameters that are of importance with respect to radioiodine collection filter cartridges are provided in Table III below:

#### **TABLE III**

### **Key Parameters of Radioiodine Collection Filter Cartridge Efficiencies**

- 1) Adsorbent bed thickness
- 2) Flow rate of pollutant stream passing through filter
- 3) Temperature of pollutant stream
- 4) Specific pollutant species
- 5) Relative humidity of pollutant stream
- 6) Type of adsorbent
- 7) Mesh size of adsorbent in filter
- 8) Sample duration
- 9) Bed compaction

Nuclear industry standards, which are applicable to the testing of nuclear grade gas phase adsorbents for radioiodine adsorption capabilities are contained in ASTM D 3803, 1989. These standard test procedures, as modified, have been utilized by F&J SPECIALTY PRODUCTS, INC. to establish the radioiodine collection cartridge efficiency performance criteria for filter cartridges manufactured by F&J. The standard ASTM D 3803, 1989 test conditions are listed in Table IV below.

### TABLE IV ASTM D 3803, 1989 PARAMETERS

1)	Pressure	1 atm
2)	Temperature	30°C
3)	Pre-equilibration Period	16 hours
4)	<b>Equilibration Period</b>	120 minutes
5)	CH <sub>3</sub> I concentration (I-131)	$1.75 \text{ mg/m}^3$
6)	Loading Duration	60 minutes
7)	Post Sweep Period	60 minutes
8)	Bed Depth	2"
9)	Velocity of Gas Stream	11.6 to 12.8 m/min.
10)	Relative Humidity	95%

F&J modifies ASTM D 3803, 1989 for its radioiodine cartridge-testing program in the following manner:

- 1) The 2" bed depth is modified to the bed depth of the specific filter cartridge geometry
- 2) Variable flow rates are utilized to determine the relationship of radioiodine collection efficiency vs. flow rate for each specific filter cartridge manufactured by F&J.
- 3) Various sample durations were utilized to represent typical field sampling scenarios of short-term grab sampling, daily sampling and weekly sampling.
- 4) F&J also measures the pressure drop at the test flow rate and develops curves and equations which illustrate the relationship of differential pressure as a function of flow rate for different adsorbent media.

TABLE V
TEST CONDITIONS FOR F&J SAMPLING SCENARIOS

PARAMETERS	SHORT-TERM	INTERMEDIATE-TERM	LONG-TERM
Pre-equilibration period (hrs.)	None	16	16
Equilibration period (hrs.)	None	2	2
Loading duration (hrs.)	1	1	1
Post sweep duration (hrs.)	1	1	168
CH <sub>3</sub> I concentration (mg/m <sup>3</sup> )	1.75	1.75	1.75
Pressure (atm)	1	1	1
Bed depth	Actual filter	Actual filter	Actual filter
Flow rate	~14 to 198 LPM	~14 to 198 LPM	~14 to 198 LPM
Temperature (°C)	30	30	30
Relative Humidity (%)	90-95	95	95

**NOTE:** Actual filter cartridges, randomly selected from stock, that are offered for sale to customers were utilized for these tests in lieu of only testing the adsorption media in a standardized fixture having a bed depth of 2".

### C. Analysis of Testing Data

The F&J program began in 1984; thus data has been accumulated for many batches of adsorbent materials.

F&J determines equations that represents the data of collection efficiency vs. flow rate and has available graphical curves and equations for CFM and LPM flow rate values.

Typical equations for TEDA impregnated charcoal and silver zeolite cartridges are presented in Appendix D. These equations for efficiency vs. flowrate curves are generally quadratic equations. They represent for the most recent multiple batch equations in CFM and LPM units. These equations apply to only F&J products and cannot be utilized for products made by other companies.

The differential pressure vs. flow rate equations are also quadratic equations. Refer to Appendix E for a typical graphical representation of a pressure vs. flow rate curve for a TEDA impregnated charcoal filter.

#### III. Factors Affecting Efficiencies of Radioiodine Collection Cartridges

Several trends for efficiencies test data have been established with respect to radioiodine adsorption characteristics of radioiodine collection cartridges manufactured by F&J. These trends are listed in Table VI below:

#### **TABLE VI**

- (A) Species Impact Collection efficiency of I<sub>2</sub> is greater than the collection efficiency of CH<sub>3</sub>I (g)
- (B) Temperature Impact
  Efficiency increases with an increase in temperature of the air flow
- (C) Relative Humidity Impact Efficiency decreases with an increase in relative humidity
- (D) Flow Rate Impact Efficiency decreases with increase in flow rate
- (E) Bed Depth Impact Efficiency increases with an increase in bed depth of the cartridge
- (F) Sample Duration Impact Efficiency generally decreases with an increase in sample duration
- (G) Particle Size Impact Efficiency increases with a decrease in particle size of the adsorbent

To illustrate the impact of several of the above parameters on collection efficiency, refer to the data illustrated in the following graphs.

Graphs A-1 and A-2 are plots of radioiodine collection efficiency vs. flow rates for four different mesh sizes of TEDA impregnated carbons and three different mesh sizes of silver zeolite in a similar filter cartridge geometry. As expected, the CH<sub>3</sub>I efficiency decreases with increasing flowrate and the efficiency is greater for the smaller particle size material at any particular flow rate.

Graphs B-1 and B-2 are plots of radioiodine efficiency vs. flow rate for three different sampling scenarios utilizing a specific TEDA impregnated carbon and Silver Zeolite, respectively, in the same filter cartridge geometry.

Graph C-1 is a plot of radioiodine efficiency vs. flow rate for two different bed depths utilizing the same filter geometry with respect to area, adsorbent and mesh size. The greater bed depth has the greater efficiency, as expected. The TE3.5M cartridge (1.62" bed depth) and the TE3M cartridge (1.0: bed depth) are compared in this example.

#### IV. F&J Quality Assurance and Quality Control Program

F&J has merged its former 10CFR50 Appendix B and NQA-1, 1994 QA programs into the internationally recognized ISO 9001 Quality Management System (Refer to Appendix F for a copy of F&J's certification). F&J also has implemented a quality process control analysis into its manufacturing operations. Key parameters that are monitored in this program are cartridge diameter, cartridge height and cartridge weight. Typical data collected on a daily basis is illustrated by Appendix F.

F&J subsequently evaluates the data to determine if product quality is within acceptable criteria and determines what action is required to continually improve the manufacturing process.

The Quality Process Control analysis also includes defect analysis. The types of rejects encountered in the manufacturing process are identified and quantitatively documented. From this analysis action is taken to implement methods to further reduce the defects by either (1) improving the compatibility of the components (2) improving operating/manufacturing procedures or (3) improving in the quality of the assembly personnel by implementing new training procedures and training sessions. Refer to Appendix G for an illustration of a typical data collection sheet for defect analysis.

The filter cartridge utilized in the General Atomics (Sorrento Electronics) Wide Range Gas Monitors are generally the model M geometry (2  $\frac{1}{2}$ "D ×1"H) and the M.5 geometry (2  $\frac{1}{2}$ "D × 1"H).

The WRGM radioiodine collection filters quality control monitoring includes the following:

- 1) 100% QC on diameter and height criteria
- 2) ~3% QC on weight criteria
- 3) 100% QC on visual inspection of key parameters
- 4) ~10% on leakage test
- 5) 100% QC on underfill/overfill inspection

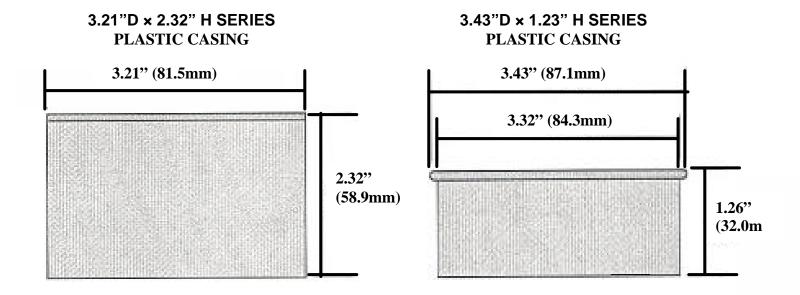
F&J individually seals each filter cartridge in a 4 mil polybag identifying the model number, the mesh size, the batch number and shelf life expiration date. The color coded labels also indicate the mesh size of the TEDA impregnated carbon filters.

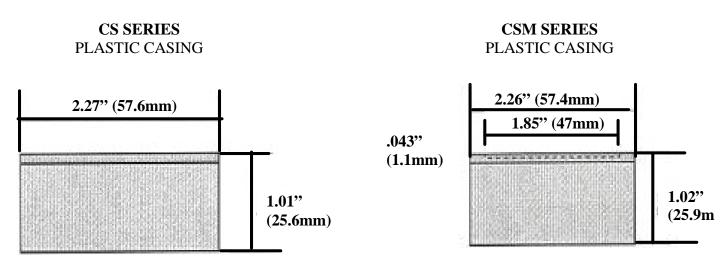
F&J's objective in its filter manufacturing process is to produce high quality filter cartridges, which have consistent and reproducible characteristics that are technically supported by good documentation detailing their radioiodine collection efficiencies vs. flow rate.

All of F&J's plastic cased TEDA impregnated charcoal filters are incineration approved by GTS Duratek and bear the incineration label on the filter.

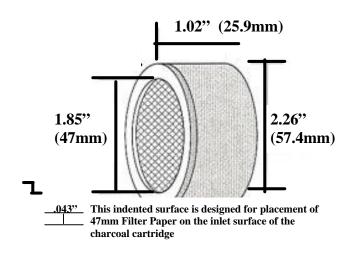
# AppendixA

### **F&J Filter Dimension Diagrams**





**CSM SERIES**ISOMETRIC VIEW



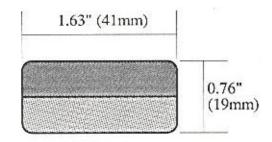
### VICTOREEN MONITOR FILTER **MODEL FJ744-FJ844**

PLASTIC CASING

### 1.24" (31mm) 1.11" (28mm)

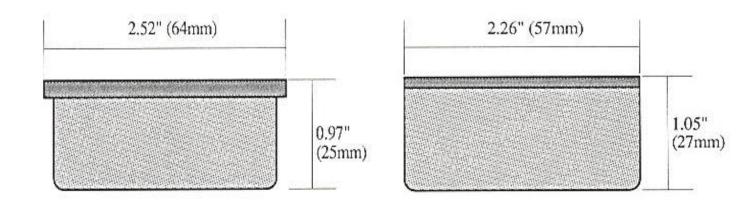
### LAPEL MONITOR FILTER **MODEL FJ433-FJ434**

PLASTIC CASING



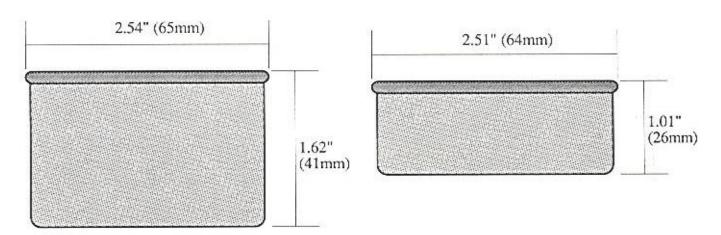
#### **MODEL "B" SERIES** PLASTIC CASING

**MODEL "C" SERIES** PLASTIC CASING



**MODEL "M.5" SERIES** METAL CASING

**MODEL "M" SERIES METAL CASING** 





### **Graphical Representation of Particle Sizes**

### **Activated Carbon Particulate Selector**

To determine approximate mesh size of an activated carbon sample, compare representative particles of the largest and smallest size to the printed solid circles. Mesh size is given in two numbers, e.g., "6x10." The first number is a mesh slightly larger than the largest representative particle, and the second is a mesh slightly smaller than the smallest particle. Normal manufacturing tolerances allow for a few non-representative particles in each sample.

STANDARD	MESH	OPE	NING	PARTICLE				
Tyler	U.S.	mm.	inches					
4	4	4.70	0.185	•				
6	6	3.33	.131	•				
8	8	2.36	.094	•				
10	12	1.65	.065	•				
12	14	1.40	.056	•				
14	16	1.17	.047	•				
16	18	0.991	.039	•				
20	20	.833	.033	•				
24	25	.701	.028	•				
28	30	.589	.023	•				
32	35	.495	.020	•				
35	40	.417	.016	•				
42	45	.351	.014	•				
48	50	.295	.012	•				
60	60	.246	.0097	•				
80	80	.175	.0069	·				
100	100	.147	.0058					
150	140	.104	.0041					
200	200	.074	0029					
250	230	.061	.0024					
325	325	.043	.0017					
400	400	.038	.0015					

## Appendix 6

Typical Specifications for TEDA Impregnated Charcoal and Silver Zeolite Cartridges

# TECHNICAL SPECIFICATIONS TEDA IMPREGNATED CHARCOAL FILTERS 2-1/4" D X 1" H F&J PRODUCT CODE: TE3C



CHARCOAL MESH SIZE: 20 X 40 Mesh

CHARCOAL TYPE: Coconut Shell Carbon

TEDA IMPREGNATION: 5% By Weight

**DIMENSIONS:** D = 2.26'' + /- 0.01''

H = 1.05" + /- 0.01"

CASING: Plastic Cased

FILTER LABELING: Color coded YELLOW to distinguish it

from other material types and indicating

flow direction.

PERFORMANCE TEST DATA: % CH<sub>2</sub>I vs. flow rate from 0.5 CFM to

10 CFM as per ASTM D 3803-1989.

QUALITY ASSURANCE REQUIREMENTS: ISO 9001-1994 QA PROGRAM

Statistical process control program for

diameter and height parameters.

INDIVIDUAL FILTER PACKAGE: Sealed Individually in plastic bags with

Model #, Batch # ID and mesh size. The

expiration date is labeled on the bag.

INTERMEDIATE PACKAGING: 50 Filters/Box (6 lbs.)

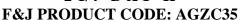
EXTERIOR PACKAGING: 200 or 250 Filters/Case (24 or 30 lbs.)

INCINERATION APPROVAL: Yes

By: GTS Duratek

Oak Ridge, TN

### TECHNICAL SPECIFICATIONS SILVER ZEOLITE 2-1/4" D X 1" H





ADSORBENT MESH SIZE: 30 X 50 Mesh

ADSORBENT TYPE: Silver Zeolite

SILVER IMPREGNATION: 37% Ag By Weight

**DIMENSIONS:**  $D = 2.26'' \pm 0.01''$ 

H = 1.05'' + 0.01''

CASING: Plastic Cased

FILTER LABELING: Color coded BLUE to distinguish it from other

material types and indicating flow direction.

PERFORMANCE TEST DATA: % CH<sub>3</sub>I vs flow rate from 0.5 CFM to

5 CFM as per ASTM D3803-1989.

QUALITY ASSURANCE REQUIREMENTS: ISO 9001-1994 QA PROGRAM

Statistical process control program for

diameter and height parameters.

INDIVIDUAL FILTER PACKAGE: Sealed Individually in plastic bags with

Model #, Batch # ID and mesh size. The expiration date is labeled on the bag.

INTERMEDIATE PACKAGING: 50 Filters/Box (6 lbs.)

EXTERIOR PACKAGING: 200 or 250 Filters/Case (24 or 30 lbs.)

INCINERATION APPROVAL: N/A

# Appendix D

### Typical Equations for Efficiency vs. Flow Rate for F&J Products

### **Equations for Methyl Iodide Collection Efficiency vs. Flowrate for**

### **TEDA Impregnated Charcoal Cartridges and Silver Zeolite Cartridges Applicable to Series C, CS, CSM, B and M**

### **Short-Term Sampling Scenario**

Adsorbent Type	<b>X</b> = <b>CFM Equations</b>	X = LPM Equations
AGZ58	$y = -0.3725x^2 + 0.8855x + 99.328$	$y = -0.0005x^2 + 0.0313x + 99.328$
TEDA-1	$y = 0.3845x^2 - 7.1557x + 106.04$	$y = 0.0005x^2 - 0.2529x + 106.04$
TEDA-2	$y = -0.4758x^2 + 0.8722x + 99.689$	$y = -0.0006x^2 + 0.0308 + 99.689$
TEDA-3	$y = -0.1253x^2 - 3.4068x + 101.52$	$y = -0.0002x^2 - 0.1188x + 101.54$
TEDA-4	$y = -1.06x^2 + 3.43x + 97.24$	$y = -0.0013x^2 + 0.1212x + 97.24$

### **Intermediate-Term Sampling Scenario**

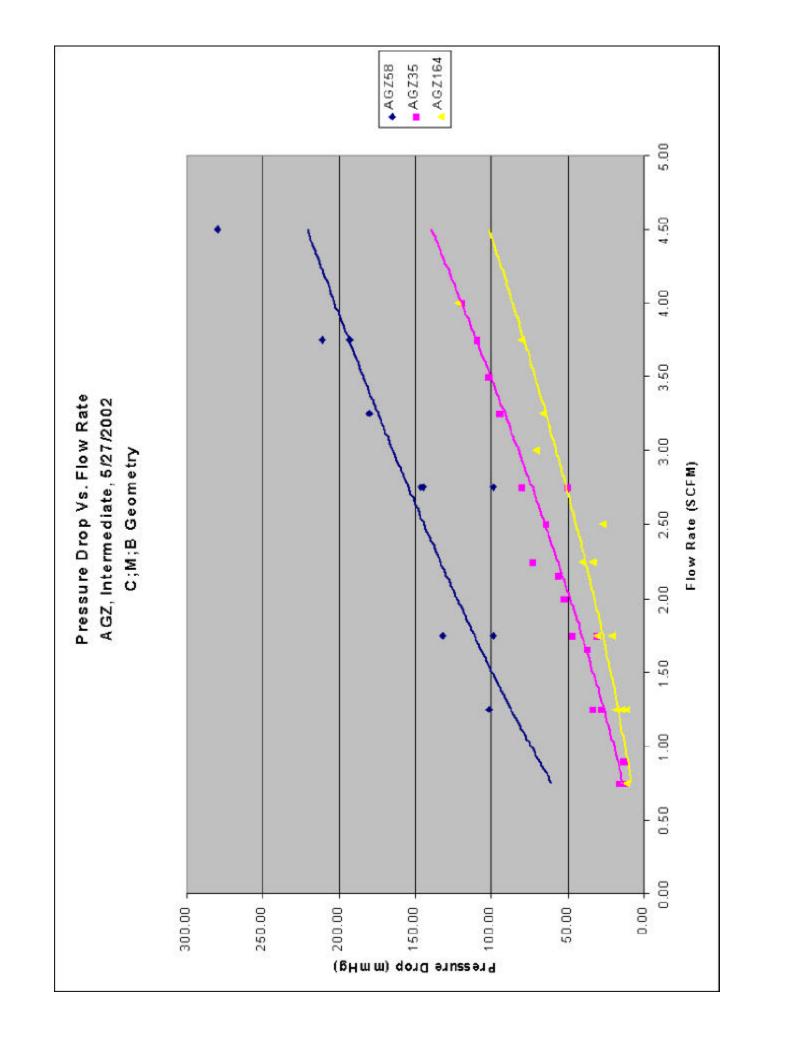
<b>Adsorbent Type</b>	X = CFM Equations	X = LPM Equations
AGZ164 AGZ35 AGZ58 TEDA-1 TEDA-2 TEDA-3 TEDA-4	$y = 0.2946x^{2} - 7.2553x + 105.73$ $y = 0.0845x^{2} - 4.0033x + 103.36$ $y = 0.39x^{2} - 1.4622x + 101.06$ $y = 1.8549x^{2} - 20.107x + 107.86$ $y = 0.2646x^{2} - 0.3535x + 100.45$ $y = 0.0467x^{2} - 4.3026x + 104.13$ $y = 3.5938x^{2} - 26.102x + 110.58$	$y = 0.0004x^{2} - 0.2562x + 105.73$ $y = 0.0001x^{2} - 0.1414x + 103.36$ $y = -0.00007x^{2} - 0.018x + 100.36$ $y = 0.0023x^{2} - 0.7102x + 107.86$ $y = -0.0003x^{2} - 0.0125x + 100.45$ $y = 0.00006x^{2} - 0.1519x + 104.13$ $y = 0.0045x^{2} - 0.922x + 110.59$

### **Long-Term Sampling Scenario**

Adsorbent Type	X = CFM Equations	X = LPM Equations
TEDA-1 TEDA-2 TEDA-3 TEDA-4	$y = 2.295x^{2} - 20.365x + 103.33$ $y = -0.1414x^{2} - 0.3481x + 99.923$ $y = -0.4928x^{2} - 1.3921x + 100.91$ $y = -1.22x^{2} - 6.23x + 100.49$	$y = 0.0029x^{2} - 0.7192x + 103.33$ $y = -0.0002x^{2} - 0.0123x + 99.923$ $y = -0.0006x^{2} - 0.0492x + 100.91$ $y = -0.0015x^{2} - 0.2211x + 100.52$

## Appendix E

### Typical Graphical Representation for Differential Pressure vs. Flow Rate





### Typical Quality Control Data Collected Regularly During Production

### F&J QA INSPECTION SHEET $\underline{\text{STI-2}}$ STRUCTURAL TESTING INSPECTION FOR METAL FILTERS

TIME: 8:00 ALL	AMOR PM	GH, CORRECTED, INITIALED, A F&J BATCH / LO	DT# <u>T-2524</u>			
DATE: 01-10-0	02	PRODUCT COD	E TE3M			
CHECK MEASURING DEVI	CES BEFORE AND AFTER MEASURE	NG RANDOM SAMPLE OF PRODU	ICTION RUN			
STANDARD: 1.0000		.00000 IN. STAND	ARD: 100.00 g			
STANDARD'S SERIAL #: 9320	92 STANDARD'S SERIAL#: 9	40171 SEF	RIAL #. B			
MEASURED / . DOC	MEASURED	MEASI	RED LUE: 100.00 g			
CALIPER'S SERIAL #: 00		SCALE'S SERIAL #:				
GEOMETRY CAN:	MI PL#IM65		PL#IM689.44			
ODOMBITE? CANA	HEIGHT (INCHES)	DIAMETER (INCHES)	WEIGHT (GRAMS)			
1	1.0185	2.5180	58.49			
2	1.0160	2.5170	58.72			
3	1.0155	2.5165	58.92			
4	1.0150	2.5150	58.52			
5	1.0125	2.5185	58.68			
6	1.0175	2.5170	58.23			
7	1.0130	2.5190	58.29 -			
8	1.0150	2.5170	59.04			
9	1.0165	2.5185	58.44			
10	1.0180	2.5160	58.83			
AVERAGE:	1. 0158	2.5173	58.62			
DESIGN RANGE;	1.01 ± -01	2.51 ±.01				
MAXIMUM:	1.0185	2.5190	59.04			
MINIMUM:	1.0125	2.5150	58.23			
RANGE:	0.0060	0.0040	0.81			
ACCEPTABLE (Y/N)	ТУ	Y	У			
I.00000" CALIPER MEASURED VALUE: /• 000	MEASURED .	LIPER CHECK 100 MEASUR • 0000 IN. VALI	160 50			
DAILY RESULTS: # PRODUCED: 5/7		# GOOD: 50	0			
# DEFECTIVE: 17		% DEFECTIVE:	The same of the sa			
DEFECTS: (BY QUANTITY			-			
UNDER FILLED: 8	OVERFILLED	CRACKED LID:				
UNDERSIZE DIA:	OVERSIZE DIA:		SIZE HEIGHTO			
COMPLETED BY (INITIALS	Marin Sanzas		-10-02			
PRODUCTION SUPERVISOR	R (INITIALS): Au	DATE:/-	-10-02			



**Typical Defect Analysis Data Collection Sheet** 

F&J QA DEFECT DATA LOG DEFECT DATA LOG FOR METAL FILTERS

5		70 /30	20/10	1/02	100								COMPLITED BY
O 4 7 Q	N O Y	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	] 	2 = =		α	-	_	•	-	,		ED BY
9 8	Ĭ,	X	Z	Σ		-							0
PN	12375	FT 2375	FI 2375 R. R. M. G. 155/	F12375								9	Yaun S
N K	R.R. A	ASK.	R.P.	P.R. F.									1
PAPER DIA. & THICK	2000	25155	15125	R.R.M 62351								\	Jansa
ASSEMBLED ITEM P.N.	1 <u>E</u> 3n	TE3H	17	TE 3H						1			1
TOTAL OTV PRODUCE D	509	507	E3M 507	515									
TOTAL QTV GOOD	500	500	500	500									
TOTAL OIV OF DIFFECT S	6	2 2	7	57									
% DEFECTIVE	1.76%	1.38%	1.38	3:41%									
LEAKAG	0	\$	p	$ \phi $									
UNDER		8	M	00									01-10
OVER FILL	p	\$	\$	\$									-
OVER SIZE DIA.	6	p	p	$\phi$									00
OVER SIZE HEIGH	8	7	8	2									
SCREEN TRAPPE D	8	\	B	$\phi$									
OTHE R		\$	0	1		_	$\perp$	L			1		

Page Lof L

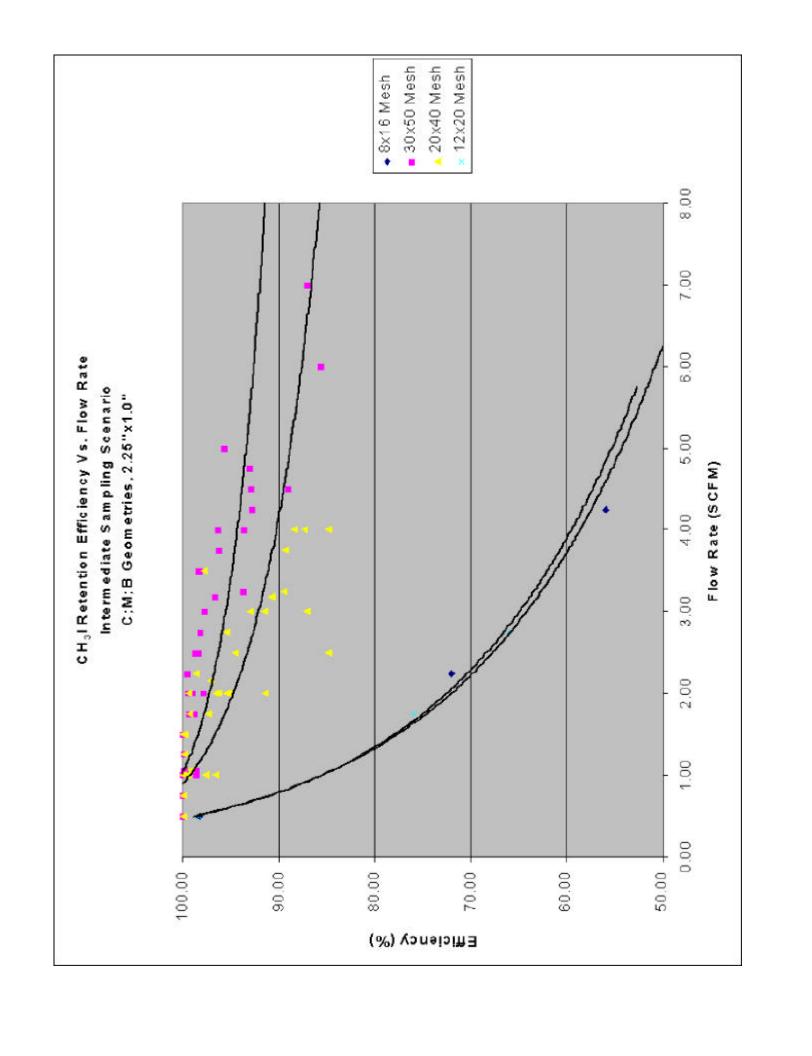
POWIN Rev 2 5,26 2000

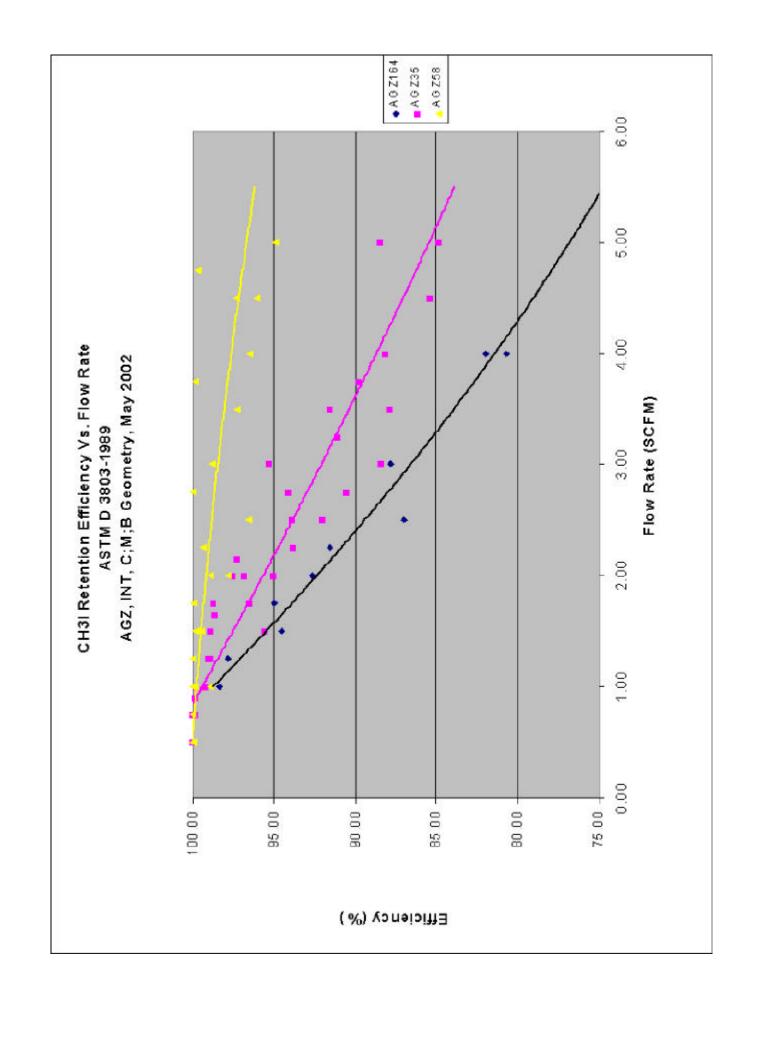
•

## Graph A-1 and A-2

# A-1 Graphical Representation of CH<sub>3</sub>I Collection Efficiency vs. Flow Rate for Four Different Mesh Sizes of TEDA Carbons

A-2
Graphical Representation of CH<sub>3</sub>I Collection Efficiency
vs. Flow Rate for Three Different
Silver Zeolite Mesh Sizes

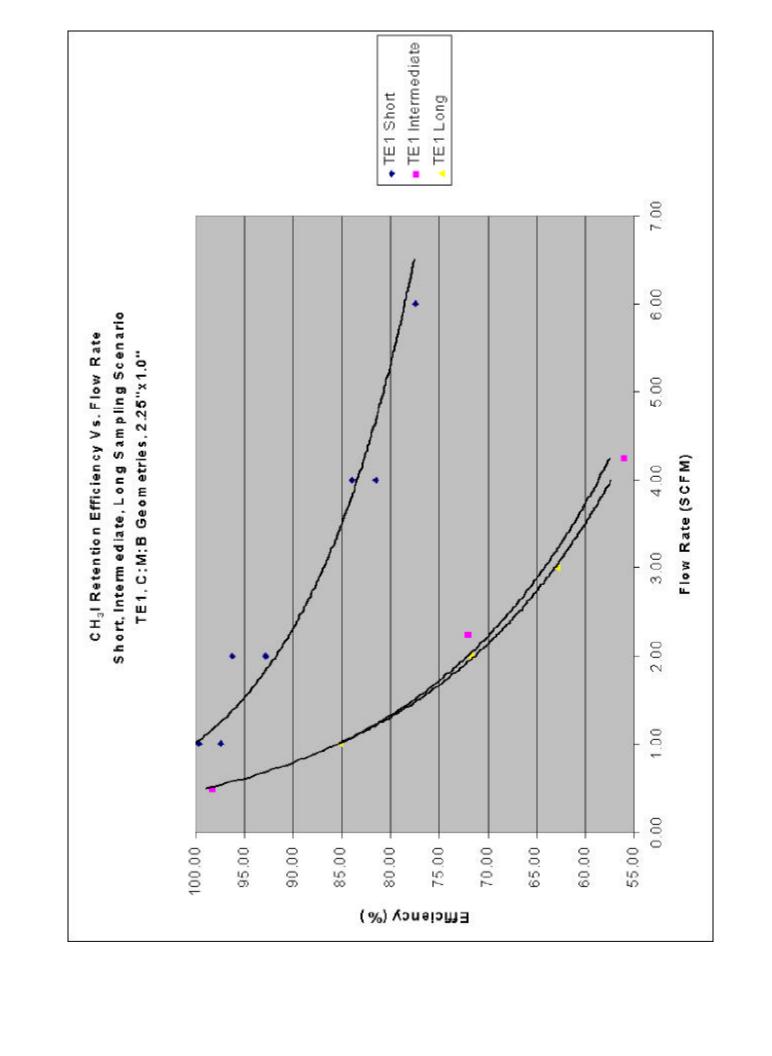


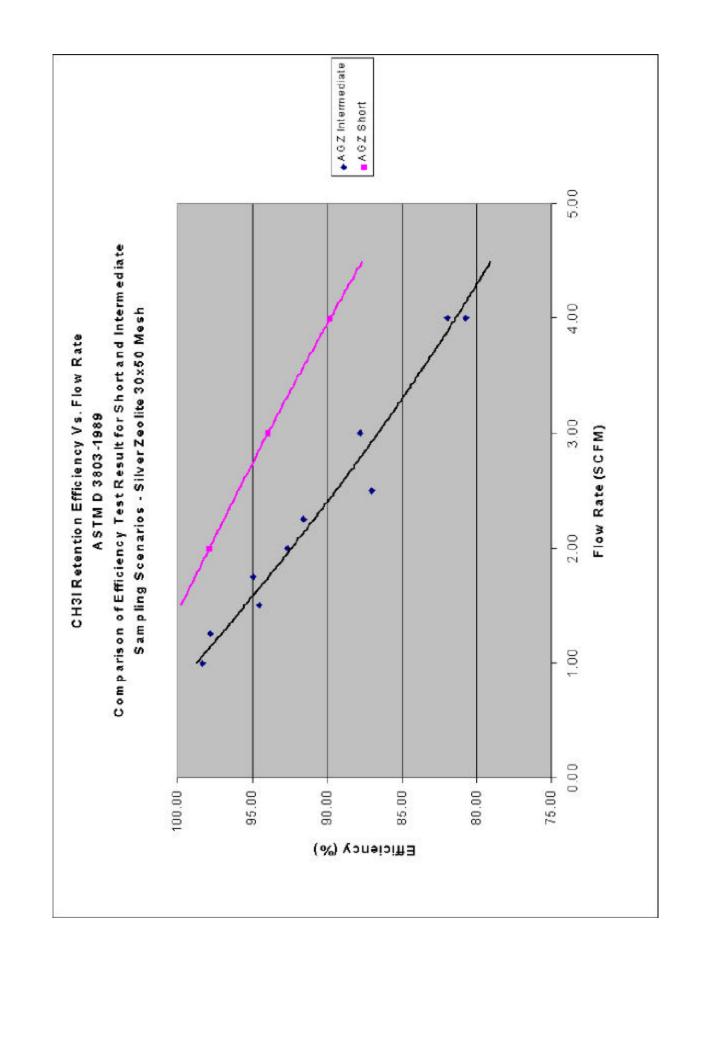


## Graph B-1 and B-2

# B-1 Graphical Representation of CH<sub>3</sub>I Collection Efficiency vs. Flow Rate for Three Different Sampling Scenarios for TEDA Carbon

B-2
Graphical Representation of CH<sub>3</sub>I Collection Efficiency vs.
Flow Rate for Two Different Sampling Scenarios for
Silver Zeolite







### Graphical Representation of Radioiodine Collection Efficiency vs. Flow Rate for Two Different Bed Depths Utilizing the same Filter Geometry

